notes

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1 Using HOM Spacing Measurements to Check Various Thermal Actuator Coupling Factors

1.1 Laying out the problem

We have a slurry of known parameters in the IFO's cold state (no Ring Heaters or self-heating), and with some measurements of the Higher Order Mode spacing (HOM) we can constrain or calculate the values of coupling factors of self-heating and ring heater power to surface curvature changes.

Table of physical parameters we know in the **cold** state:

Parameter	Symbol	Value	Unit
ITMY Radius of Curvature	$R_{ m i, c}$	$1939.2 \\ 2246.9 \\ 3994.47$	m
ETMY Radius of Curvature	$R_{ m e, c}$		m
ARM Length	L		m

1.2 Cavity g-factors

We can relate the cavity g-factor (a measure of the test masses' curvature relative to the cavity length) to the HOM spacing data.

Here is a list of symbols used in the derivation:

Parameter	Symbol
ITM g-factor	g_i
ITM g-factor, cold-state	$g_{i,c}$
ETM g-factor	g_e
ETM g-factor, cold-state	$g_{e,c}$
Round-trip Gouy Phase	ψ_{rt}
Curvature, cold-state (ITM, ETM)	$D_{i,c}, D_{e,c}$
Curvature, hot-state (ITM, ETM)	D_i, D_e
Self-heating curvature coupling (ITM, ETM)	A_i, A_e
Ring-heater curvature coupling	B
Self-heating power (ITM, ETM)	$P^i_{\text{self}}, P^e_{\text{self}}$
Ring-heater power (ITM, ETM)	$P^i_{\rm rh}, P^e_{\rm rh}$

To start we relate the HOM spacing to the cavity g-factor:

$$\begin{split} f_{\rm HOM} &= \frac{\psi_{rt}}{2\pi} f_{\rm FSR} \\ \psi_{rt} &= 2 \arccos{(\sqrt{g_i g_e})} \\ g_i g_e &= \cos^2{\left(\pi \frac{f_{\rm HOM}}{f_{\rm FSR}}\right)} \end{split}$$

Then we express the test mass g-factors in terms of the thermal contributions

$$\begin{split} g_i &= 1 - LD_i, \quad D_i = D_{i,c} + A_i P_{\text{self}}^i + BP_{\text{rh}}^i \\ g_e &= 1 - LD_e, \quad D_e = D_{e,c} + A_e P_{\text{self}}^e + BP_{\text{rh}}^e \end{split}$$

Multiplying them together and assuming second order terms are small:

$$\begin{split} g_i g_e &= 1 - L \left(D_{i,c} + D_{e,c} + A_i P_{\text{self}}^i + A_e P_{\text{self}}^e + B(P_{\text{rh}}^i + P_{\text{rh}}^e) \right) \\ &+ L^2 \left(D_{i,c} D_{e,c} + D_{i,c} (BP_{\text{rh}}^e + A_e P_{\text{self}}^e) + D_{e,c} A_i P_{\text{self}}^i + \ (A_i A_e + (A_i + A_e) B + B^2 \text{ terms}) \right) \end{split}$$

The terms on the right side are assumed to be small and negligible.

$$\begin{split} g_i g_e &= 1 - L(D_{i,c} + D_{e,c}) + L^2 D_{i,c} D_{e,c} - L\left(A_i P_{\text{self}}^i + A_e P_{\text{self}}^e + B P_{\text{rh}}^e\right) \\ &+ L^2 \left(D_{i,c} (B P_{\text{rh}}^e + A_e P_{\text{self}}^e) + D_{e,c} A_i P_{\text{self}}^i\right) \end{split}$$

We can gather terms by groups of cold state terms, B depedent terms, and self-heating terms:

$$\begin{split} g_i g_e &= G_c - BLP_{\rm rh}^e(1-LD_{i,c}) + X_s = G_c + X_s - BLP_{\rm rh}^e g_{i,c} \\ &\cos^2\left(\pi\frac{f_{\rm HOM}}{f_{\rm FSR}}\right) = G_c + X_s - BLP_{\rm rh}^e g_{i,c} \\ &G = G_c + X_s - BLP_{\rm rh}^e g_{i,c} \end{split}$$

where,

$$\begin{split} G_c &= 1 - L(D_{i,c} + D_{e,c}) + L^2 D_{i,c} D_{e,c} = g_{i,c} g_{e,c} \\ X_s &= -L \left(A_i P_{\text{self}}^i (1 - L D_{e,c}) + A_e P_{\text{self}}^e (1 - L D_{i,c}) \right) = -L \left(A_i P_{\text{self}}^i g_{e,c} + A_e P_{\text{self}}^e g_{i,c} \right) \end{split}$$

1.3 Fitting data to recover *B* and constrain X_s

By fitting a line (y = mx + b) to the HOM data as a function of $P_{\rm rh}^e$, we can recover the HOM change due to self heating as well as the coupling of ring-heater power to curvature (B):



2 Using TCS SIM value to project its estimate of HOM spacing shift due to self heating.

OMC Data estimate of HOM spacing shift due to self-heating alone: 174.6 Hz, from 5166.1 Hz --> 5340.7 Hz

TCS SIM estimate of HOM spacing shift due to self-heating alone: 451.5 Hz, from 5166.1 Hz --> 5617.7 Hz

Difference Factor : TCS_SIM / OMC_DATA = 2.59

3 Use curvefit and HWS data for ITM absorption estimates to estimate hot-state ARM qs

Using TCS-SIM ITMY surface defocus from self-heating gain (-3.65e-05 D/W), ETMY surface defocus is 3.56e-06 diopters in order to have the same HOM spacing shift from self-heating as observed. The ratio of ETMY / ITMY surface defocus from self-heating gain is 0.80 The defocus above is positive ... indicating the ITMY surface defocus gain or absorption is too high. If we use an ITMY surface defocus from self-heating gain of -1.38e-05 D/W, we get ETMY surface defocus of: -8.98e-07 diopters And this yields a ETMY surface defocus from self-heating gain of -1.11e-05 D/W, and a gain ratio of 0.80 if we assume that the absorption is the same as that of the ITMY. The corresponding value in TCS-SIM is -2.93e-05 D/W. Measured HOM spacing in the XARM: 5312.50 Hz Predicted HOM spacing in the XARM: 5324.86 Hz With the following assumed parameters: Pxarm: 3.852e+05 Pyarm: 3.852e+05 alpha_yi: 3.750e-07 alpha_xi: 4.300e-07 beta: 0.000e+00 B: 7.755e-07 L: 3.994e+03 gyic: -1.060e+00 gyec: -7.778e-01 gxic: -1.059e+00 gxec: -7.799e-01 Gxc: 8.257e-01 Gyc: 8.243e-01 Pyirh: 0.000e+00 Pyerh: 2.146e+00 Pxirh: 8.500e-01 Pxerh: 1.950e+00 Gx: 8.149e-01 Gy: 8.198e-01 alpha_e: 2.100e-07 Solution for Ai (self-heating to surface defocus gain): -2.571e-05 D/W Calculated mismatch at BS of 0.428% for the following parameters: Pxarm: 385159

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Pyarm: 385159
alpha_yi: 3e-07
alpha_xi: 6e-07
beta: 0.8
Larm: 3994.47
B: 7.75e-07
itmx_static_curvature: 0.0005153842189352162
etmx_static_curvature: 0.00044559308439533023
itmy_static_curvature: 0.0005156765676567656
etmy_static_curvature: 0.00044505763496372776
itmx_static_lens: -1.2e-05
itmy_static_lens: 1.7e-06
Pyirh: 0
Pyerh: 2.146
Pxirh: 0.8
Pxerh: 1.95
co2y_power: 1.716
co2y_to_sub_dfs: -1.3e-05
itmy_rh_to_sub_dfs: -9e-06
itmy_self_heating_sub_dfs_gain: 0.000487
itmy_thickness: 0.19957
co2x_power: 1.711
co2x_to_sub_dfs: -1.1e-05
itmx_rh_to_sub_dfs: -9e-06
itmx_self_heating_sub_dfs_gain: 0.000487
itmx_thickness: 0.19957
Ai: -2.33e-05
alpha_e: 1.0344e-07
n: 1.45
bs_thickness: 0.0604
bs_aoi: 0.7853981633974483
ITMY_to_BS: 5.3328
ITMX_to_BS: 5.3828
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